



Mathematical Modelling, Design, and Optimization of Electrochemical Capacitors from Layered Materials

INNOCENT S. IKPE^{a,b,d}, Iakovos Sigalas^{a,b}, Sunny Iyuke^a and Kenneth I. Ozoemena^{a,b}

^a School of Chemical & Metallurgical Engineering and DST-NRF Centre of Excellence in Strong Materials, University of the Witwatersrand, Johannesburg, South Africa

^b Materials for Energy Research Group (MERG), University of the Witwatersrand, Johannesburg, South Africa

^c Department of Chemical Engineering, Federal University of Technology Owerri Nigeria,

^d CSIR Materials Science and Manufacturing, Pretoria, South Africa

and ^e School of Chemistry, University of the Witwatersrand, Johannesburg, South Africa



INTRODUCTION

Electrochemical Capacitors (ECs) are electrical energy storage devices that store charges through either electrostatic charging of a double layer or through a Faradaic reaction or through both mechanisms. It has higher energy density than conventional electrostatic capacitors and as well higher power density than batteries in general. The key performance parameters of electrochemical capacitors are specific capacitance, energy density, power density, rate capability and cycling stability [3].

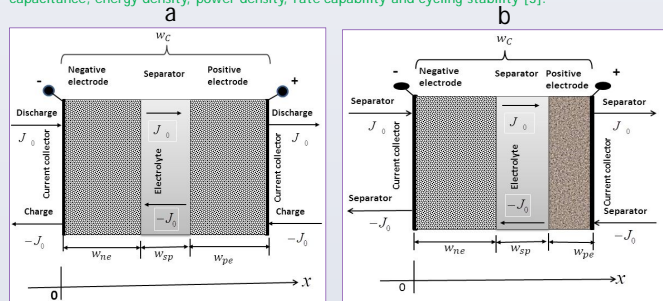


Figure 1. (a) symmetric electrochemical capacitor cell, (b) asymmetric electrochemical capacitor cell showing various functional layers on the macroscale [1].

AIMS AND OBJECTIVES

The aims of this study is to develop mathematical models for various of ECs and build theoretical basis to examine the effects of self-discharge, operating conditions and design configurations on the Performance of the devices. To also optimize the ECs design parameters and operating conditions for high energy and power performances. Also to develop a realistic guideline for design optimal design of ECs enhanced performance parameters like specific energy, power density, lifecycle and energy retention

THE MATHEMATICAL MODELS

$$\begin{aligned} \frac{\partial \phi_{we}(x,t)}{\partial t} &= \beta \frac{\partial^2 \phi_{we}(x,t)}{\partial x^2} + \frac{J_{vr}(x,t)}{C_v} \\ \beta^2 &= \frac{\alpha_1 \alpha_2}{C_v (\alpha_1 + \alpha_2)} \\ J_{vr}(x,t) &= J_{vr1}(x,t) + J_{vr2}(x,t) \\ \rho C_p \frac{\partial T(x,y,z,t)}{\partial t} &= \nabla \cdot (k_{x,y,z,t} \nabla T(x,y,z,t)) + Q_{ec}(x,y,z,t) \end{aligned} \quad \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \end{matrix}$$

RESULTS AND DISCUSSIONS

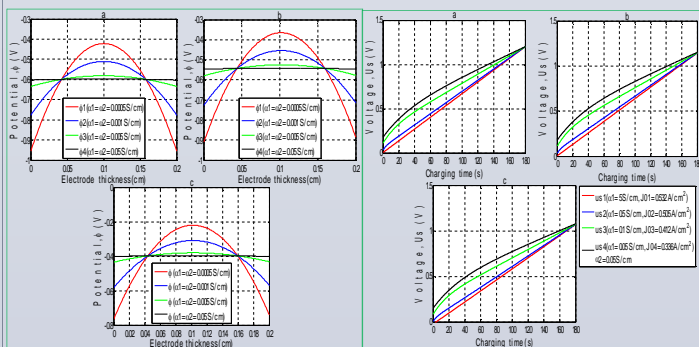


Figure 2: Electrode potential profiles as a function of position after charge process for (a) EC without self-discharge (b) EC with self-discharge due to only EDLs instability and (c) EC with self-discharge due to both side-reactions/redox reactions and EDLs instability

Figure 3: EC voltage dependence on time during charge process from 0V to 1.2V for (a) EC without self-discharge (b) EC with self-discharge due to only EDLs instability and (c) EC with self-discharge due to both side-reactions/redox reactions and EDLs instability

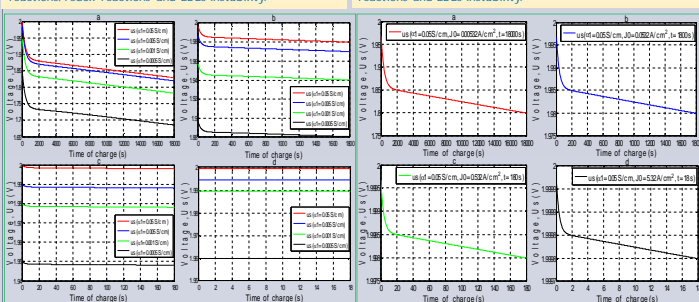


Figure 4: The voltage decay of asymmetric ECs of various electrodes effective conductivity over time by self-discharge due to both side-reactions/redox reactions and EDLs instability for charge process from 0.8V to 2.0V. (a) 18000s charging, (b) 1800s charging, (c) 180s charging and (d) 18s charging.

Figure 5: The voltage decay of asymmetric ECs over time by self-discharge due to both side-reactions/redox reactions and EDLs instability for charge process from 0.8V to 2.0V. (a) 18000s charging, (b) 1800s charging, (c) 180s charging and (d) 18s charging.

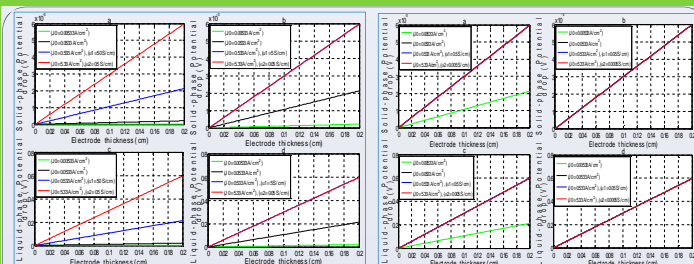


Figure 6. Solid-phase potential drop for ECs charged at various current densities and of electrode and electrolyte effective conductivity (a1 & a2) of (a) 50S/cm & 0.5S/cm, (b) 5S/cm & 0.05S/cm, liquid-phase potential drop for ECs charged at various current densities and of a1 and a2 of (c) 50S/cm & 0.5S/cm, (d) 5S/cm & 0.05S/cm.

Figure 7. Solid-phase potential drop for ECs charged at various current densities and of effective conductivity (a1 & a2) of (a) 50S/cm & 0.05S/cm, (b) 0.05S/cm & 0.005S/cm, liquid-phase potential drop for ECs charged at various current densities and of a1 and a2 of (c) 50S/cm & 0.05S/cm, (d) 0.05S/cm & 0.005S/cm.

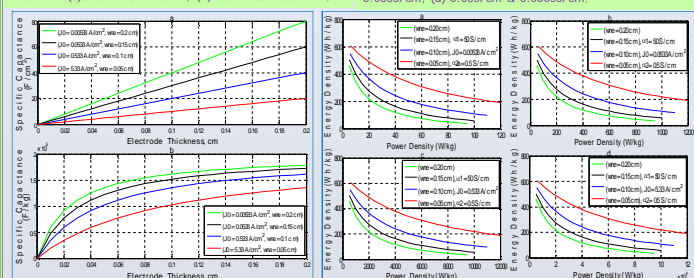


Figure 8. Ragone plots of ECs with various effective conductivities a1=50S/cm, a2=0.5S/cm charged at (a) 0.00533A/cm² for 18000s, (b) 0.0533A/cm² for 1800s, (c) 0.533A/cm² for 180s, and (d) 5.33A/cm² for 18s.

Figure 9. Ragone plots of ECs with various effective conductivities a1=50S/cm, a2=0.5S/cm charged at (a) 0.00533A/cm² for 18000s, (b) 0.0533A/cm² for 1800s, (c) 0.533A/cm² for 180s, and (d) 5.33A/cm² for 18s.

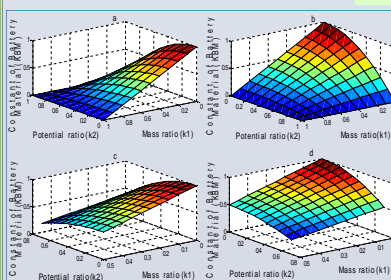


Figure 10. Profile of the value of K_B as a function of the mass and operating potential window ratio factors of the battery-kind electrode for 3-D side view of ratio factors of the battery-kind electrode for 0 < k1 ≤ 1 and 0 < k2 ≤ 1 limits and (b) front of 0 < k1 ≤ 1 and 0 < k2 ≤ 1 limits and (c) side of 0 < k1 ≤ 0.5 and 0 < k2 ≤ 0.7 limits and (d) front of 0 < k1 ≤ 0.5 and 0 < k2 ≤ 0.7 limits

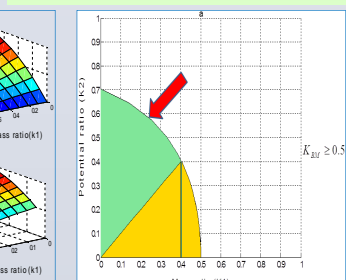


Figure 11. Profile of conditions of k1 and k2 for higher values of both energy and power density of asymmetric ECs EDLs and PDs, in comparison with the values of energy and power density of symmetric ECs EDLs and PDs.

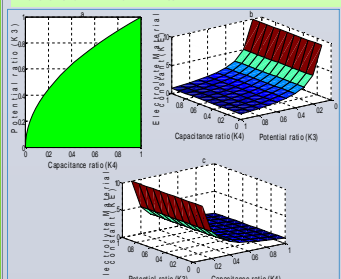


Figure 12. (a) Profile of the given condition of K_E ≥ 1.0 as a function of k3 and k4 ratios; (b) front view of the value of electrolyte material-associated constant K_E as a function of k3 and k4 ratios; and (c) side view of the value of K_E as a function of k3 and k4 ratios.

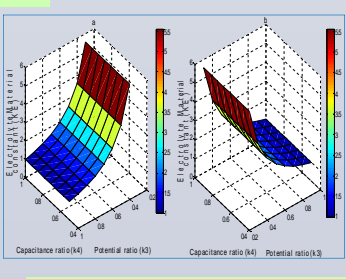


Figure 13. (a) Profile of the value of K_E as a function of k3 and k4 ratios for ranges of 0.3 ≤ k3 < 1 and 0.5 ≤ k4 < 1; and (b) 3-D side view profile of the value of electrolyte material-related constant K_E as a function of k3 and k4 ratios for ranges of 0.3 ≤ k3 < 1 and 0.5 ≤ k4 < 1.

CONCLUSIONS

ECs with self-discharge loss some of the storable energy as self-discharge during the device charging and discharging processes. Charging and discharging the device fast reduced the rate of the self-discharge. The amount of current density that should be employed to successfully charge ECs is greatly dependent on the effective conductivities of the electrode and electrolyte as well as electrodes thickness. Therefore, ECs of low electrode and electrolyte effective conductivities cannot be charged effectively at high current density, because potential drops in the liquid-phase will be as high as half the cell's voltage. The typical length scale (w₀) over which liquid potential drop occurs can be employed as design parameter to optimize electrodes thickness for ECs designed to function under a given current density spans. Ragone plots of ECs with diverse electrode thicknesses and different effective conductivities a1 and a2 charged at different current densities can be utilized to select electrode dimensions to attain a given energy and power density specifications. Asymmetric EC with suitable electrode mass and operating potential range ratios has over two-fold E_{ec}, E_{ec}, E_{ec}, E_{ec}, and P_{ec} higher than those of symmetric EDLC using the same aqueous electrolyte. Also, asymmetric EC proper electrode mass and operating potential range ratios joined with appropriate organic electrolyte has over five-fold E_{ec}, E_{ec}, E_{ec}, and P_{ec} higher than those of similar asymmetric EC using aqueous electrolyte. These results can be a great guideline for design, fabrication and operation of EC of outstanding performance in terms of high energy and power densities.